



UNIVERSITY OF MALTA
FACULTY OF ENGINEERING
B.ENG.(HONS.) IN MECHANICAL ENGINEERING
YEAR III – SEMESTER I
JANUARY/FEBRUARY 2013 SESSION OF EXAMINATIONS

MEC 2307 – Thermodynamics II

19th January, 2013

13:00 – 16:00 hours

*This paper contains **SIX** questions. You are to attempt **FIVE**.*

Stationery: Use of calculators is allowed
 Steam Tables

1. Gases expand in a propulsion nozzle from 3.5 bar and 425 °C down to a back pressure of 0.97 bar, at the rate of 18 kg/s. Calculate the required throat and exit areas of the nozzle assuming negligible inlet velocity and isentropic flow.

For the gases take $\gamma = 1.333$ and $c_p = 1.11 \text{ kJ/kgK}$.

If a coefficient of discharge of 0.99 and a nozzle efficiency of 0.94 are considered, what would be the throat and exit areas?

(20 marks)

2. The ultimate analysis (by mass) of a sample of petrol was : C 83%; H 14%; O₂ 3%. If the dry products had 1 % CO, calculate:
 - (a) the stoichiometric A/F ratio
 - (b) actual AFR
 - (c) the analysis of dry products for the rich operation
 - (d) the volume ratio of H₂O in the exhaust and the temperature to which the gas must be cooled before condensation of the H₂O vapour begins, if the pressure in the exhaust pipe is 1.013bar.

(20 marks)

3. In a diesel cycle, air at 1bar and 15°C is compressed isentropically. Heat is then added at constant pressure to 1200°C. The compressed air is expanded isentropically to its initial volume and finally cooled at constant volume to its initial temperature. The compression ratio is 16. Sketch the $p-v$ diagram for this cycle. Find the work output per kg of air, the heat engine efficiency and the mean effective pressure.

(20 marks)

4. (a) Show that for a reciprocating air compressor

$$W_i = \frac{n}{n-1} \dot{m} R T_1 \left\{ \left(\frac{p_2}{p_1} \right)^{(n-1)/n} - 1 \right\}$$

(8 marks)

- (b) A single-stage, double acting air compressor is required to deliver 14 m³ of air per minute measured at the inlet conditions of 1.013 bar and 15°C. The delivery pressure is 7 bar and the speed 300 rev/min. Take the clearance volume as 5% of the swept volume with a compression and re-expansion index of $n = 1.3$. Sketch the $p-v$ diagram. Calculate the swept volume of the cylinder, the delivery temperature, and the indicated power.

(12 marks)

5. (a) Show that the efficiency for a Joule Cycle, (ideal GT cycle) with a constant c_p and γ throughout the cycle, is given by:

$$\eta = 1 - \frac{1}{r_p^{(\gamma-1)/\gamma}}$$

Where r_p is the pressure ratio, and mass flow is constant throughout cycle, *i.e.* neglect mass of fuel flow.

(10 marks)

- (b) A GT Cycle works with a pressure ratio of 12. The minimum and maximum temperatures in the cycle are 30°C and 1000°C. The compressor isentropic efficiency is 80% while the turbine isentropic efficiency is 90%. For the compression of air $\gamma = 1.4$ and $c_p = 1.005$ kJ/kgK while for the combustion and expansion processes $\gamma = 1.3$ and $c_p = 1.15$ kJ/kgK. Calculate
- the heat input
 - the heat rejection
 - the work ratio
 - the overall efficiency

(10 marks)

6. (a) A vapour compression refrigerator using R12 works between temperature limits of -5°C and 40°C . The refrigerant enters the compressor dry saturated and is at 9.607 bar downstream of the compressor. Calculate the refrigeration effect and coefficient of performance if the refrigerant is sub-cooled to 20°C before entering the throttling valve. If a cooling effect of 3 kW is required, what is the amount of heat rejected from the condenser.

(10 marks)

- (b) In a regenerative steam cycle employing one open feed heater the steam is supplied to the turbine at 42 bar and 500°C and is exhausted to the condenser at 0.035 bar. The bleed steam for feed heating is taken at a pressure of 4 bar. Sketch the Ts diagram. Assuming ideal processes and neglecting feed pump work, calculate:
- the fraction of the boiler steam bled for feed heating
 - the power output of the plant per unit mass flow rate of boiler steam
 - the cycle efficiency

(10 marks)

Additional information

$$\frac{T_1}{T_2} = \left(\frac{v_2}{v_1} \right)^{n-1} \quad \text{and} \quad \frac{T_1}{T_2} = \left(\frac{p_1}{p_2} \right)^{(n-1)/n}$$

$W = \frac{(p_2 v_2 - p_1 v_1)}{n-1} = \frac{R(T_2 - T_1)}{n-1}$ where W is specific work, p is pressure and v specific volume, n is the polytropic index, R is the specific gas constant and T is the temperature. Subscripts 1 and 2 refer to the states.

$$s_2 - s_1 = c_p \ln \left[\frac{T_2}{T_1} \right] + R \ln \left[\frac{p_1}{p_2} \right]$$

$$\frac{p_c}{p_1} = \left(\frac{2}{\gamma + 1} \right)^{\frac{\gamma}{\gamma - 1}}$$

Where p_c is the critical pressure for a nozzle, p_1 is the upstream pressure, and γ is the ratio of specific heats i.e. c_p/c_v

$$C_c = \sqrt{\gamma R T_c}$$

$$\text{Nozzle Efficiency} = \frac{C_2^2 - C_1^2}{C_{2s}^2 - C_1^2}$$

$$\text{Velocity Coefficient} = \frac{C_2}{C_{2s}}$$